# The Arc Loss Challenge: A Novel Industrial Benchmark for Process Analytics and Machine Learning

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#### Abstract

Rapid development in data-driven process monitoring has provided a rich selection of models and data preprocessing strategies for applications such as fault detection and diagnosis. However, the development, comparison, and selection of process monitoring algorithms can become complicated and unnecessarily onerous. As a result, numerous publicly available benchmark datasets have emerged in the literature. Unfortunately, benchmark literature often suffers from problems such as low fidelity, inconsistent usage, and lack of transparency. This paper presents a benchmark challenge based on a large-scale industrial dataset that aims to enhance the evaluation and comparison of learning algorithms and overall data preprocessing workflows. We introduce the arc loss challenge, a machine learning benchmark with data from a large-scale mining and pyrometallurgy operation. By providing a supervised learning challenge based on large quantities of raw industrial process data with transparent and consistent evaluation procedures, the arc loss challenge is a unique contribution to fault detection benchmarking.

*Keywords:* Benchmarking, Big data analytics, Fault detection and diagnosis, Machine learning, Process monitoring, Pyrometallurgy

## 1 1. Introduction

Benchmarking has allowed the process systems engineering (PSE) community to make
valuable contributions toward addressing problems related to process monitoring, including fault detection and diagnosis (FDD). Benchmark datasets are of great value to the
community as they form the basis for developing, testing, and comparing different algorithms for process monitoring. In addition, benchmark datasets have played a critical role
in advancing the field by enabling direct progress tracking of proposed methods [1].

The literature on data-driven methods for FDD often relies on idealistic simulated datasets 8 to evaluate monitoring algorithms. Unfortunately, this approach makes it difficult to comg pare the practical utility of different algorithms [2, 3, 4]. In addition, recent advances 10 in computational hardware and algorithmic efficiency have made traditional FDD bench-11 mark datasets, released decades ago, seem "simple and easy to solve." For example, the 12 widely used Tennessee Eastman process (TEP) dataset [2] has been solved with increas-13 ingly accurate results (96% to 100%) using advanced machine learning (ML) algorithms 14 [5]. Therefore, a turn toward modern benchmarks incorporating raw industrial data is 15 essential to provide a realistic platform for data-driven process monitoring. 16

This paper aims to improve process monitoring benchmark research by introducing the arc 17 loss challenge, an ML benchmark with operating data from a pyrometallurgy plant. It con-18 sists of one year of daily exports from multiple sources, including process measurements, 19 valve positions, and laboratory measurements. The dataset captures many of the non-20 trivial challenges faced by industrial practitioners, such as multimodality, class imbalance, 21 and irregular sampling rate. The arc loss challenge also provides the PSE community with 22 an open-source competition for fault detection with standardized evaluation procedures to 23 facilitate the comparison of different fault detection workflows. 24

The arc loss benchmark dataset can be downloaded from the arc loss challenge website. 25 The website contains the raw data stored in Apache Parquet (.parquet) files and standard-26 ized testing software. The testing software is designed to establish consistency, encourage 27 transparency, and prevent over-fitting by providing a rigorous evaluation procedure to com-28 pare different monitoring workflows. The main contributions of the arc loss challenge are 29 as follows: i) to provide a publicly available dataset from an industrial process historian, 30 ii) to present a formal procedure for consistently evaluating submissions to track progress 31 in FDD, iii) and to facilitate more impactful research in FDD. 32

This paper is organized as follows: in Section 2, background information is provided to differentiate the arc loss challenge from existing FDD benchmarks; in Section 3, we present the metallurgical process in question, Section 4 introduces the arc loss challenge, Section 5 describes the dataset, Section 6 provides insights and observations from the industrial data, Section 7 reviews the submission and evaluation procedures and why these procedures were chosen, and Section 8 presents a demonstration of how the benchmark dataset can be used for the development of FDD workflows. Finally, the paper ends with concluding remarks in Section 9.

## **2. Benchmarking in Process Monitoring**

Since its release in 2010, the ImageNet dataset [6] has provided the computer vision com-42 munity with a benchmark dataset to develop and test proposed models. In turn, the accu-43 racy of the state-of-art model has catapulted from 50.90% to 90.88% in just 11 years [7]. 44 This rapid growth in computer vision was partly enabled by the community-wide adoption 45 of an open-source standardized dataset (i.e., ImageNet dataset). Over the same period, the 46 data available for FDD has grown substantially due to the increased digital transformation 47 of the process industries. This section briefly reviews existing FDD benchmark datasets 48 and places the arc loss benchmark dataset relative to other works. 49

In general, FDD benchmark datasets fall into two categories depending on the method 50 used for data acquisition. The first category is simulated data or data that is artificially 51 generated to replicate the real-world but with known underlying patterns [8]. Simulated 52 data exists on a spectrum ranging from low fidelity to high fidelity, depending on the 53 degree of precision and realism portrayed in the simulation models [9]. For example, sim-54 ulation models based solely on first-principles (e.g., TEP [2, 10] and PenSim [11, 12]) 55 exhibit a low level of fidelity. This is because such models tend to omit real-world char-56 acteristics and model them as Gaussian random variables or linear piece-wise functions. 57 Next, simulation models for process equipment and instrumentations are derived from 58 the analytical description of the physical behaviour of the equipment, such as thermo-59 dynamics and mechanics. For instance, the DAMADICS (Development and Application 60 of Methods for Actuator Diagnosis in Industrial Control Systems) benchmark provides a 61 simulation model of electro-pneumatic actuators in a sugar production process [13]. To 62 more accurately represent the real-world effects, hybrid models integrate measurements 63 from a real process with the simulation models. Hybrid models (e.g., CSTH [14]) provide 64 a platform for FDD applications under realistic conditions of measurement noise, process 65 disturbances and constraints [15]. 66

Real-world data constitute the second category and are obtained from an actual process.
Real-world data can be acquired from one or more sources. Possible data sources include
readings from physical sensors, alarm events, laboratory results, valve positions, images,

and video records. For instance, the PRONTO benchmark [16] includes heterogeneous 70 data from disparate sources in an industrial-scale multi-phase flow facility. In contrast, the 71 3W benchmark [17] only includes eight process measurements related to the operation of 72 offshore oil wells. The heterogeneity of real-world data presents a number of opportunities 73 and challenges for robust and reliable FDD applications. Figure 1 shows a conceptual 74 comparison of some of the most prominent FDD benchmarks. For a more comprehensive 75 analysis and comparison of accessible benchmarks for process monitoring, readers can 76 refer to the review paper by Melo et al. [18]. 77



Figure 1: A conceptual comparison of several FDD benchmarks available in the literature. The following criteria are used to compare the benchmarks: 1) the origin of the data (simulations or actual physical sensors), 2) the number of features, 3) the number of classes, 4) the type of simulation models in the case of simulated data, and 5) the heterogeneity of the data in the case of real-world data. The size of blobs is proportional to the number of classes; a legend is displayed in the top left corner, spanning from 2 to 20 classes. Both plots share the same y-axis.

In the PSE community, the first form has become more prevalent than the second. This 78 is due to the difficulty of acquiring high-quality data with recurring and identifiable faults 79 in industrial settings [19]. For instance, i) industrial processes often have an inherently 80 long mean time between failures (MTBF) [20], ii) faults often prevent operation entirely, 81 and iii) most data owners refuse to publish open-source data due to confidentiality and 82 intellectual property concerns [18]. As a result, most faults in existing FDD benchmark 83 datasets are artificially induced by abnormally deviating a characteristic property of the 84 underlying simulation models. In this work, we present a novel benchmark challenge that 85 we believe will have a significant impact on FDD research, similar to the positive impact 86

that the ImageNet challenge had on computer vision. The arc loss benchmark dataset,
obtained from three different data sources - process measurements, valve positions, and
lab results - falls under the category of real-world data.

## **3.** Pyrometallurgical Smelting Process

The arc loss benchmark dataset was acquired from a large-scale open pit mine and pyrometallurgical plant. The high-level mining and pyrometallurgical operations are depicted in Figure 2. In such processes, high-grade oxidized ore deposits are converted into
refined base metals to be processed by shotting and packaging units before being shipped
to customers [21]. In this section, the relevant mining and pyrometallurgical operations are described.



Figure 2: An illustration of the broader mining and metallurgical processes [22].

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Saprolite ore is mined from multiple open pits in the massif using hydraulic shovels. The extracted ore is then loaded onto dumper trucks and transported to the ore preparation plant. Due to the friable nature of the run-of-mine ore, waste rocks and undersized particles are removed via crushing and screening operations in the ore preparation plant [23]. The crushed ore is conveyed on an overland belt conveyor to the metallurgical plant, where it is further processed.

Figure 3 shows a simplified schematic of the metallurgical plant in question. Processing 103 operations such as milling, drying, calcining, reduction, and smelting are used in the met-104 allurgical plant. Ore from the preparation plant is wet (i.e., it has a moisture content of up 105 to 40%); therefore, the ore is dried as the first step in the metallurgical plant [24]. Ham-106 mer mill flash dryers are used to produce fine ore with less than 1% free moisture content. 107 Next, the dried ore is fed into a series of calciner cyclones operating at 1000 °C where it 108 is dehydrated [25]. The calcined ore is then pre-reduced in fluidized bed reducers using 109 pulverized coal and hot gases at 1000  $^{\circ}$ C to remove oxides [26]. This step is critical to 110

ensure the operational stability of the subsequent smelting operation in the direct current
 electric arc furnace (DC EAF) unit. The focus of this challenge is on the operation of the
 DC EAF utilized as a smelter to refine ores into base metals.



Figure 3: A simplified schematic process flow diagram

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A schematic diagram of the DC EAF is illustrated in Figure 4. The smelter unit consists 114 of a refractory-lined cylindrical vessel with water-cooled sidewalls, a conical roof, and a 115 twin hollow graphite electrode located vertically in the center of the roof [27]. The steel 116 vessel contains a molten mixture with a dense metal phase below a lighter slag phase. 117 Refined ore is fed to the furnace through multiple feed ports positioned on the roof using 118 weight bin feeders (c.f., Figure 5). The slag and metal are tapped intermittently from the 119 furnace through launders. Two plasma arcs span from the bottom tip of the electrodes 120 to the top surface of the molten bath, serving as cathode and anode, respectively. The 121 graphite electrodes are connected to a large DC power supply, providing the electrical 122 power required for the DC EAF unit operation [28]. 123

<sup>124</sup> The high-temperature plasma arcs are developed by means of the direct electrical current



Figure 4: A typical view of the DC EAF unit.

transfer from the cathodes to the anode. The arcs serve as the main heating component in 125 the DC EAF unit [27]. The plasma arcs convert the electrical energy attained from the DC 126 power supply (up to 80 MW) into thermal energy (above 1500 °C) required to maintain the 127 metal-to-slag ratio at desirable operating levels [29]. Since the operation of the DC EAF is 128 directly related to the thermal energy transferred into the molten bath, the presence of the 129 plasma arcs is critical to ensure operational stability and maximum production efficiency. 130 However, the loss of the plasma arc is an unforeseen process fault that adversely impacts 131 the efficiency and stability of the DC EAF unit. 132

# **4.** Problem Definition for the Arc Loss Challenge

This section defines the process fault and its impact on the operation. In addition, an overview of the principal challenge is provided.



Figure 5: Top furnace view of feed ports.

#### **4.1.** The process fault: loss of furnace plasma arc

The arc in the DC EAF is a plasma-based jet with a high temperature and velocity that conducts electricity efficiently [30]. It serves as the primary heating element in the DC EAF, transforming electrical energy from the DC power supply into thermal energy and transmitting it into the molten bath. The DC electric circuit running through the furnace connects the arc and slag bath in series, splitting the total operating voltage between them depending on the electrical properties of the slag (i.e., electrical resistivity) [27].

The slag is often of high electrical resistivity, resulting in a significant voltage drop across the slag layer of the circuit [31]. As a result, the available voltage could be less than the required voltage for the arc to develop, leading to an arc loss event. Other suspected causes of arc loss include upstream process disturbances, electrical disturbances, and extra-long arcs.

<sup>148</sup> Due to the harsh process conditions and safety-critical nature of the operation, obtaining <sup>149</sup> a visual recording of the plasma arc is infeasible in this scenario. Therefore, the daily <sup>150</sup> raw exports have no arc loss labels. Fortunately, unexpected power fluctuations can help <sup>151</sup> define arc loss events. Specifically, a loss of arc in an electrode at time *t* occurs if and only <sup>152</sup> if the following three conditions related to its power are satisfied: i) a power drop of 10 <sup>153</sup> MW or more relative to the one recorded at t - 0.6 min, ii) the power must be steady for <sup>154</sup> approximately 11.25 minutes within a standard variation of 2 MW before the power drop



Figure 6: Timeline chart of power and arc loss conditions

(i.e., from t - 11.85 min to t - 0.6 min), and iii) the power must return to within  $\pm 5$  MW of the initial stable range in approximately 9.85 minutes after the power drop (t + 9.25min) [32]. Figure 6 illustrates the three conditions that constitute an arc loss event. For each sample, these conditions are used to produce output labels that are binary indicators of an arc loss (i.e.,  $0 \rightarrow$  no arc loss and  $1 \rightarrow$  arc loss) in the corresponding electrode.

The unexpected occurrence of arc loss severely impacts the DC EAF. In addition to having an effect on electrical efficiency, recovering from an arc loss often requires a temporary feed reduction and a power increase. Figure 7 illustrates the severity of the arc loss event on the process. It displays a side-by-side comparison of the process measurements recorded during stable and faulty operating regimes. Since the DC EAF operation is directly related to the presence of an open arc, having a reliable predictive alarm that alerts operators of the onset of arc loss would be of great economic and environmental value.

#### <sup>167</sup> 4.2. Arc loss prediction: a supervised learning challenge

The proposed benchmark fuses data preprocessing, feature engineering, supervised learning, and fault detection into a single challenge. Most of the existing FDD benchmarks investigate the use of conventional and advanced ML on clean simulated data. The proposed challenge offers a different form of contribution as it focuses on comparing and validating end-to-end data analytics workflows on raw historical data taken from a largescale industrial process. Figure 8 illustrates the typical layout of an FDD process analytics



Figure 7: Visual demonstration of the arc loss on the process operation. The left-hand plot represents a relatively stable operation, while the right-hand plot represents a faulty operation. The time t marks the time at which an arc loss event occurred. Both plots share the same y-axis. Readers are referred to Table A1 for variables' descriptions.

workflow. Note that there may also be hidden feedback connections between the modules
 as such frameworks often progress iteratively.

The objective of this challenge is to utilize information from a full year of high-frequency operating data to correctly predict the onset of an arc loss event (i.e., the target variable Y). For the purpose of this challenge, the target variable Y is defined as an event where either one of the following conditions is satisfied: i) a loss of the arc in electrode A only, ii) a loss of the arc in electrode B only, or iii) arc losses in both electrodes A and B. Mathematically speaking, Y can be described as follows:

$$Y = \begin{cases} 0, & A^{Loss} + B^{Loss} = 0\\ 1, & A^{Loss} + B^{Loss} > 0 \end{cases}$$
(1)



Figure 8: Typical structure of an overall process analytics workflow for FDD.

where  $A^{Loss}$  and  $B^{Loss} \in [0, 1]$  are binary indicators of an arc loss in electrodes A and B respectively. The target variable Y has been pre-computed as part of the minimal preprocessing performed on the dataset.

## **5.** Industrial Data for the Arc Loss Challenge

The raw data consists of one year of high-frequency operating data collected from various metallurgical process units (e.g., calcining, smelting, reduction, etc.). This section summarizes the process parameters and pre-processing methods carried out to make the data easier to use.

#### 190 5.1. Data structure

Each raw daily export captures a day of operation in 2022 and is stored with over 200 191 columns and roughly 30,000 rows. The columns in the daily exports correspond to pro-192 cess variables (PVs) and their associated timestamps. As shown on the left-hand side of 193 Figure 9, the PV sampling rates vary. The number of samples collected from a particular 194 PV throughout the day is represented by the number of rows (i.e., the height of blue and 195 red bars). Some PVs have high-frequency measurements (e.g., a sample every three sec-196 onds), while laboratory measurements can have sampling periods greater than three hours. 197 Overall, the total daily exports have an uncompressed size of 17.4 gigabytes (GB), making 198 the data unwieldy for practitioners to load, analyze, and process. 199

In addition to the varying sampling rates, the raw data is riddled with other problematic artifacts such as bad inputs, outliers, and irrelevant or misleading data. The arc loss benchmark is concerned with workflows that take in raw data and yield models that pro-



Figure 9: Illustration of structuring a raw daily export

vide operational insights and predictions. Therefore, the arc loss dataset published with this paper is available in a raw form with minimal pre-processing to structure the data.

To make the data easier to utilize, we pre-processed all raw daily exports to follow a struc-205 tured format where all PVs have a unified timestamp. As illustrated in Figure 9, data struc-206 turing was performed by identifying the most frequently sampled PV and using the cor-207 responding timestamp as a reference to reindex the remaining PVs. The unified sampling 208 frequency is three seconds. Additionally, all PVs with categorical values were replaced by 209 numerical indicators (e.g., close and open became 0 and 1, respectively). Finally, prob-210 lematic entries (e.g., tag not found, access denied, bad data, etc.) were substituted with not 211 a number (NaN) values. 212

Overall, the data consists of a time index and 111 PVs. Although it is too much information to present here, the tag, description, range, and unit of measurement for each PV are provided in Table A1. There are 92 PVs with high-frequency samples representing physical process properties (e.g., feed rate, temperature, etc.), 14 variables with discrete values (label encoded) that correspond to valve positions, and five laboratory measurements with a sampling period greater than one hour.

#### **5.2.** Accessing the arc loss data

For the purpose of this challenge, the data is chronologically split into training/validation (Jan.-Oct.) and testing (Nov.-Dec.) sets. The daily exports are bundled and stored in

two compressed (.parquet) files. Participants are allowed to use any data in the training/validation set for tuning the hyperparameters of their candidate model. The arc loss
challenge data can be downloaded from here in the form of (.parquet) files:

- trainval.parquet: This 1.21 GB dataset (Jan.-Oct.) is intended for training
   and validating the process monitoring workflows
- 227 2. test.parquet: This 0.60 GB dataset (Nov.-Dec.) is for testing the monitoring 228 algorithm and benchmarking with performance metrics.

### **6.** Data Exploration and Analysis

Process knowledge and data exploration can guide participants to discover valuable information for their analysis. This section provides insightful summaries and observations
regarding the industrial data and the underlying process. The content provided in this
section was collected from process experts and previous data analysis.

#### **6.1.** Dataset statistics

Table 1 summarizes relevant statistics for the arc loss benchmark dataset. Figure 10 shows 235 the daily arc loss events over an entire year of operation. It can be observed that arc loss 236 faults are most frequent from May through September. Additionally, Figure 11 presents 237 a circular graph for the arc loss rate in June. The chart displays a time series of 30 days, 238 starting from June 1<sup>st</sup>, 2022 at 00:00 at the innermost circle, and moving clockwise until 239 reaching June 30th, 2022 at 23:00 at the outermost ring. Dark blue is used to indicate 240 periods with a higher fault rate, while light blue denotes periods with the fewest faults. 241 Both Figures 10 and 11 imply that the process faults are characterized by randomness, 242 seasonality, and variability, making fault detection a non-trivial task. 243

Total number of samples	10483200
Total number of PVs	111
Sampling period	3 sec
Total number of categorical variables	14
Training/validation set ratio	83.5% (JanOct.)
Testing set ratio	16.5% (NovDec.)
Number of classes	2
Class ratio (normal:faulty)	3337:1

Table 1: Summary of arc loss dataset statistics.



Figure 10: The number of arc loss events per day throughout a year of operation



Figure 11: The distribution of arc loss events over operating hours in June



Figure 12: Statistics of the arc loss benchmark dataset.

In one year of operating data, the furnace experiences 3,141 arc loss events. As illustrated in Figure 12a, the month that saw the most arc loss events was June, closely followed by September, and October was the month that witnessed the fewest arc loss events.

Figure 12b shows that both subclasses (arc loss A and arc loss B) that constitute the faulty class (Y=1) are represented approximately equally in the arc loss data. This indicates that the arc loss event is independent of which electrode is operating. Even though arc loss events typically last less than one minute, a single arc loss fault can cause up to 10 minutes worth of production loss involving significant material and energy inefficiencies. On average, 9.4 arc loss events occur daily, resulting in 82 minutes of lost production as shown in Figures 12c and d, respectively.

#### **6.2. Process shutdowns**

A shutdown is a period of time during which a process is taken from a normal to an idle state of operation to carry out all necessary maintenance. Even though shutdowns are scheduled in advance, their duration is not known *a priori* with high certainty. If samples corresponding to shutdown periods are not carefully imputed, the trained predictive models could be biased toward an irrelevant process state. Data from shutdowns do not possess any meaningful information from the process perspective. Therefore, it is essential to identify shutdown periods to prevent model degradation.

The selection of relevant PVs for shutdown identification is a non-trivial problem and often requires the support of operators or domain experts. According to process experts, a time period  $[t_a, t_b]$  corresponds to a process shutdown period if and only if the total power (TP) drawn from both electrodes A and B are less than 10 MW (AP + BP  $\leq 10$  MW) for at least ten hours ( $t_b - t_a > 10$  hrs) as shown in Figure 13. Participants are encouraged to use their judgment and select any strategy they deem appropriate for dealing with shutdown data.



Figure 13: Illustration and quantitative definition of shut down periods.

#### **6.3.** Sampling frequency

Statistical process monitoring methods for fault detection are generally designed for uniformly sampled data. However, like any other industrial process, the pyrometallurgy process in question is a multi-rate sampling system. In other words, PVs are measured in a non-uniform fashion and differ in sampling rate. The variables with the highest sampling rates are primarily temperature-related, while those with the lowest are laboratory measurements.

Fusing multi-rate sampled process measurements has resulted in a significant amount of
missing data. Missing data are encoded as blanks or not a number (NaN) values. In fact, 38
PVs have over 90% of their values missing as demonstrated in Figure 14. The predictive



Figure 14: The distribution of missing values for PVs.

power and quality of a data-driven model can be adversely impacted by training it on data
with lots of missing values. Hence, it is important to address the missing data problem.
Participants are free to employ any data imputation technique to tackle the missing values
problem.

#### **6.4.** Observations from the data

Several observations from the dataset that might be of interest to participants when developing their monitoring algorithms are provided in the following list:

- December 1<sup>st</sup> records are missing.
- December 4<sup>th</sup> has the highest percentage of missing values, with over 83%.
- W1F, W2F, W3F, W6F, W7F, W8F, and TMF measurements are unreliable due to instrumentation errors (i.e., incorrect calibration, malfunction, etc.).
- The minimum time interval between two successive arc loss events is 10 minutes.
- PV data does not always lie within the range provided by process experts and listed in Table A1. For instance, almost all crucible heat loss data are outside the limit as shown in Figure 15. Participants may have to evaluate data quality and perform sanity checks to improve the reliability and robustness of monitoring algorithms (i.e.,

relying on process knowledge for data cleaning is not always an infallible strategy).

Different PVs are highly coupled and may exhibit strong cross-correlations. A PV may also have an autocorrelation with its previous values. These correlations reveal the underlying characteristics of the process and they may change during abnormal operations (e.g., arc loss). The electrical parameters pertaining to electrode A are depicted in Figure 16. The orange plot represents the measured voltage, while the blue plot corresponds to the theoretical voltage computed using Ohm's law. Such theoretical relationships can be used for data reconciliation to enhance data quality.



Figure 15: Box plots illustrating PV data distributions. Expected range lines are shown for each PV, normalized to be consistent with the normalized values.

#### **7.** Submission and Evaluation

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This section outlines the procedures for submitting entries to the benchmark challenge and discusses the evaluation process. The submission and scoring procedures for the arc loss challenge are designed to ensure fairness through transparency and consistency. The evaluation also aims to prevent over-fitting by emphasizing soft sensor durability over two consecutive months of unseen operating data. The following section explains how submissions are scored. We encourage participants to post their questions and queries in our community discussion forum.



Figure 16: Observations from the benchmark dataset: comparing the actual vs. theoretical voltage drawn by electrode A.

#### **7.1. Submission of entries**

The arc loss challenge is divided into two stages. Firstly, participants should use the *la*-312 *beled* training/validation set to develop a monitoring workflow, optimize hyperparameters, 313 and estimate the performance measures. In the second stage, participants are required to 314 run their workflow on the *unlabeled* testing set (Nov. and Dec. data) to classify whether 315 each timestamp in the testing set corresponds to stable operation (Y = 0) or an arc loss 316 event (Y = 1). More specifically, participants are required to only submit the timestamps 317 that belong to the faulty class (Y = 1). The scoring metric (described in subsection 7.2) is 318 computed specifically on the instances that are important for the problem, i.e., identifying 319 arc loss events. It is worth noting that since the minimum time interval between two con-320 secutive arc loss events is 10 minutes, submitted timestamps should be at least 10 minutes 321 apart. Entries must be submitted as a . zip file containing the following: 322

• A one-column . CSV file containing the predicted timestamps of arc loss events. The entries should be in the form of (yy-mm-dd hh:mm:ss) (e.g., 22-12-01 14:04:12)

To reduce the likelihood of over-fitting, we will not release the ground-truth labels of the testing set until the challenge is over. Releasing the true testing labels could lead to some "optimistic" results, where participants test several configurations on the testing set and only report the best result. This risk is present in any benchmarking initiative where the ground truth is made available.

Participants may have a maximum of 20 attempts over the course of the competition. Upon
 submission, participants will receive their performance score on the held-out testing set.
 The arc loss challenge comprises an unofficial phase and an official phase. During the

unofficial phase, participants may receive scores for up to five attempts. This will allow 333 participants to examine the testing software and compare different methodologies without 334 being officially counted for the competition. In the official phase, participants are allowed 335 to submit up to 15 attempts, and the best-performing attempt will be officially counted. 336 Note that unused attempts during the unofficial phase can not be carried over to the official 337 stage. Attempts that can not be scored due to incompleteness (e.g., improper formatting, 338 missing components, etc.) will not be counted toward the attempt limits. The challenge 339 deadlines are listed in Table 2 (check our website for further updates). The data will be 340 publicly available for approximately a year before the submission deadline. This will 341 allow substantial time for data cleaning and ensure that participants with limited access to 342 computational resources have an equal chance of winning. After the competition deadline, 343 the fully labeled data will be made publicly available to facilitate the development of data-344 driven process monitoring algorithms by the community. 345

Tuble 2. Chantenge dedalmes						
Phase	Start date	Deadline	Entry limit			
Unofficial phase	June 1 <sup>st</sup> , 2023	August 31 <sup>st</sup> , 2023	5			
Official phase	September 1 <sup>st</sup> , 2023	July 1 <sup>st</sup> , 2024	15			

Table 2: Challenge deadlines

#### 346 7.2. Scoring

Evaluating results on the two-class arc loss dataset poses several challenges, including 347 the non-uniform prior distribution across the classes, with P(Y = 0) > 0.9997 and 348 P(Y = 1) < 0.0003. For this reason, a simple performance measure like accuracy is 349 not proper because it fails to distinguish between the number of correctly classified sam-350 ples of different classes. Moreover, the cost of misclassifying a positive sample (i.e., a 351 false negative or missed alarm) is greater than the cost of incorrectly classifying a sample 352 from the negative or majority class (i.e., a false positive or false alarm). These factors must 353 be taken into account when designing a suitable scoring metric. In addition to these chal-354 lenges, it is critical to predict arc loss events before they occur to enable operators to take 355 preventive measures. Hence, a novel scoring metric is designed to address the imbalanced 356 classes and associated costs, reward early predictions, and penalize late predictions. 357

For this challenge, a binary prediction  $\hat{Y}(t)$  is made for each time step t, i.e., :

 $\hat{Y}_{N}(t) \begin{cases} \hat{Y}_{N}(t) = 0, \text{ a negative prediction at time } t \text{ during a normal operating period (N)} \\ \hat{Y}_{N}(t) = 1, \text{ a positive prediction at time } t \text{ during a normal operating period (N)} \\ \hat{Y}_{F}(t) = 0, \text{ a negative prediction at time } t \text{ during a faulty operating period (F)} \\ \hat{Y}_{F}(t) = 1, \text{ a positive prediction at time } t \text{ during a faulty operating period (F)} \end{cases}$ 

Figure 17 illustrates the scoring functions assigned to each  $\hat{Y}(t)$ . During faulty operating 360 periods (F) (i.e.,  $t_{early} \le t \le t_{late}$ ), early arc loss detection is crucial. Therefore, arc loss 361 predictions made within 7 mins before the onset time of arc loss  $t_{loss}$  are rewarded with a 362 maximum reward of (+1.0) given at  $t_{optimal} = t_{loss} - 5$  mins. However, positive predictions 363 that are more than 7 mins before  $t_{loss}$  (i.e.,  $t < t_{early}$ ) are penalized (-0.5). Additionally, 364 late arc loss predictions are unhelpful, and missed arc loss predictions are significantly 365 harmful. To reflect this, arc loss predictions made up to 2 minutes after  $t_{loss}$  (i.e.,  $t > t_{late}$ ) 366 are slightly penalized (-0.1), while no arc loss predictions or missed alarms are heavily 367 penalized (-2.0). 368



Figure 17: The scoring functions for negative and positive predictions during normal (right) and faulty (left) operating periods. True positives are rewarded based on their time stamps, while false negatives (i.e., models that fail to predict arc loss before  $t_{late}$ ) receive a penalty of -2.0. Late predictions ( $t_{loss} < t < t_{late}$ ) are slightly penalized with -0.1, and false positives are penalized with -0.5. True negatives are neither rewarded nor penalized.

During normal operating periods (N), when no arc loss events occur within 10 mins (i.e.,  $t < t_{early}$  or  $t > t_{late}$ ), false alarms can lead to decreased confidence in monitoring models and poor allocation of operational attention and resources. To address this, false alarms (i.e.,  $\hat{Y}_N(t) = 1$ ) are penalized with a score of -0.5. However, negative predictions (i.e.,  $\hat{Y}_N(t) = 0$ ) are neither rewarded nor penalized.

The total score of a model's predictions is calculated by summing the scores across all time steps t:

$$U_{total} = \sum_{t \in T} U(t) \tag{2}$$

To facilitate interpretation, we normalize Equation 2 such that all scores fall within the range [0 - 1], using the following Equation:

$$U_{normalized} = \frac{U_{total} - U_{inactive}}{U_{optimal} - U_{inactive}}$$
(3)

where  $U_{optimal}$  denotes the unnormalized optimal score while  $U_{inactive}$  denotes the unnor-378 malized score for a completely inactive classifier (no positive predictions). The highest 379 possible normalized score  $U_{normalized}$  is 1, which is awarded to the optimal model that 380 accurately predicts all arc loss events with a 5-min warning and generates no false alarms. 381 Conversely, an inactive model that only outputs negative predictions and does not detect 382 any arc loss events will receive a normalized score  $U_{normalized}$  of 0. The winner of the chal-383 lenge will be determined based on the model with the highest normalized score  $U_{normalized}$ 384 on the unseen testing set. 385

## **8.** Demonstration of an Arc Loss Prediction Workflow

This section provides a demonstration example of the arc loss prediction workflow using the benchmark dataset. The example serves as a baseline framework for the arc loss challenge. The demonstration starts with an overview of the methods used to clean the raw data. It is followed by a description of the predictive model used for workflow development and its performance evaluation. Participants can use the baseline Python implementation available on the challenge website as a template for developing their own submissions.

#### **8.1. Data preprocessing**

Data preprocessing is a crucial procedure that involves cleaning and preparing data for analysis and modelling. The quality of data preprocessing can significantly impact the generalization performance and effectiveness of the final model or analysis. When done properly, data preprocessing can enhance the accuracy of the analysis and improve the model's performance. However, inadequate data preprocessing can lead to inaccurate or biased results. In this demonstration example, data preprocessing tasks include removing outliers, handling shutdown data, imputing missing data, and scaling or normalizing data.

Outliers are data points that lie far away from the rest of the data points in a dataset. To 401 remove outliers from the raw dataset, the Z-score method was used. This method involves 402 calculating the Z-score for each data point, which is the number of standard deviations 403 away from the mean that the point lies. Data points with a Z-score greater than a specified 404 threshold were considered outliers and were replaced with NaN (Not a Number). The 405 threshold value used in this method was set to 3. Next, the data from shutdown periods 406 (i.e., periods of zero or low activity) were carefully handled using the zero-imputation 407 technique. It involves identifying periods of time during which power values are below a 408 certain threshold for more than a certain time threshold (refer to section 6.2) and replacing 409 these values with zeros. To address missing data (represented by NaN values), a forward-410 fill operation was performed. This method involves filling missing values with the last 411 measured value. However, in cases where missing values occur at the beginning of the 412 time series with no previous measurements, a backward-fill approach was used, where 413 missing values were filled with the first measured value in the time series. Finally, the 414 data were scaled to have zero mean and unit variance. The scaling was performed by 415 subtracting the mean and dividing it by the standard deviation of the training data. 416

#### **8.2.** Arc loss prediction: baseline performance

Given the binary characteristic of the problem at hand, logistic regression was chosen 418 as the natural baseline model to demonstrate the feasibility of our benchmark in validat-419 ing data-driven process monitoring workflows. Logistic regression is a widely used and 420 well-established algorithm for binary classification tasks, providing an effective and in-421 terpretable starting point for our analysis. The logistic regression model estimates the 422 probability of a time stamp belonging to the faulty class (Y = 1), using a logistic or sig-423 moid function. This probability is then converted into a binary prediction by applying a 424 threshold, typically 0.5. To address the class imbalance, cost-sensitive learning was used. 425 This involves assigning different costs to both classes during the training process inversely 426 proportional to their frequencies. Specifically, misclassifying faulty class instances (false 427 negatives) has a higher cost than misclassifying normal class instances (false positives). 428 A hold-out strategy was employed for model evaluation. The train/val set was split into 429 two subsets: a training set comprising January-August data used for training the model, 430 and a validation set comprising September-October data used for validating the models' 431 hyper-parameters. Next, a random search over a manually predefined search space is per-432 formed to find a well-performing model configuration. Finally, the model with the hyper-433 parameter configuration that achieved the best performance on the validation set during 434 the random search was tested on the testing set. 435

<sup>436</sup> Table 3 summarizes the performance evaluation of the baseline model reported on the

testing set. To assess the model's performance, we use three key terms: true positive (TP), false negative (FN), and false positive (FP) predictions. In our case, we define a TP prediction as a positive prediction made between the time interval of  $t_{early}$  and  $t_{loss}$ . On the other hand, an FN prediction is a negative prediction made during  $t \in [t_{early} - t_{loss}]$ . Finally, an FP is a positive prediction made at  $t \notin [t_{early} - t_{loss}]$ . To help illustrate a TP prediction made by the baseline model on the testing set, readers are referred to Figure 18.

Table 3: Performance evaluation of the baseline workflow. Abbreviations: TP- true positives, FP - false positives, FN - false negatives.

Basalina scora	TP	FP	FN	Precision	Recall	$F_2$	$U_{normalized}$
Dasenne score	247	499	173	0.3311	0.5881	0.5091	0.2077



Figure 18: An illustration of a TP prediction.

The baseline workflow presented in this section is intended to serve as a starting point 443 rather than a complex solution. Participants are encouraged to use it as a reference point 444 to measure and compare their own workflows. The results of the baseline demonstrate the 445 suitability of the benchmark dataset for testing data-driven process monitoring workflows. 446 The well-defined problem and well-documented faults provide a suitable testing ground. 447 For more complex solutions, readers can refer to our previous work [32] where traditional 448 and contemporary approaches to representation learning and binary classification were 449 compared in a comprehensive analysis for their ability to predict arc loss. Additionally, 450 Table 4 summarizes various approaches for addressing different challenges that can be 451 tested and validated using this benchmark dataset. By exploring these approaches, re-452

453 searchers can develop a deeper understanding of the strengths and limitations of different
 454 methods, and develop more effective and robust monitoring workflows.

Tasks	Baseline approach	Suggested methods
Outliers removal	Z-score method	Interquartile range method [33] Distance-based methods [34, 35] Domain knowledge (PV limits)
Shutdown data handling	Zero-imputation	Exclusion (removal from analysis) Integration (include in the analysis) Segmentation (separate analysis)
Missing data imputation	Forward/ backward filling	Regression imputation [36, 37] K-nearest neighbor imputation [38] DL imputation [39, 40]
Feature selection/ extraction	N/A	Dimensionality reduction [41] Embedded methods [42] Deep representation learning [43]
Fault detection & diagnosis	Linear ML model	Threshold-based methods [44] Statistics-based methods [45] DL models [46, 47]

Table 4: Comparison of baseline and suggested methods for various challenge tasks: a guide for participants

## **9.** Conclusion

The arc loss benchmark dataset is a valuable resource that contains a large amount of his-456 torical industrial data from a large-scale metallurgical process with an unexpected process 457 fault, namely an arc loss. The dataset spans an entire year of operation data collected 458 from various metallurgical process units with fast sampling rates. The paper describes the 459 process in detail and presents an overview of the data characteristics, such as data types, 460 variables, and sampling rates. Additionally, the paper introduces the arc loss challenge, 461 which is an open-source challenge that provides the community with a standardized dataset 462 and evaluation framework for comparing different industrial fault detection methods. The 463 primary objective of the arc loss challenge is to catalyze research in the fast-growing field 464 of process monitoring and FDD, and to investigate whether the success of deep learn-465 ing and ML in computer vision and natural language processing can be replicated in the 466

process industries. The authors believe that the arc loss benchmark dataset will be a valu able asset to the FDD community and will inspire new ideas for real-world industrial data
 applications.

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# 476 Appendix A. Process Variable Information

	Tag	Description	Range	Unit		
Pro	Progress parameters					
1.	t	Time [yyyy-mm-dd hh:mm:ss]				
Sme	elting paramet	ers				
2.	AP	Electrode A power	0-60	MW		
3.	BP	Electrode B power	0-60	MW		
4.	TP	Total power (AP+BP)	0-100	MW		
5.	APSP	Electrode A power set point	0-60	MW		
6.	BPSP	Electrode B power set point	0-60	MW		
7.	AC	Electrode A current	0-100	kA		
8.	BC	Electrode B current	0-100	kA		
9.	ACSP	Electrode A current set point	0-100	kA		
10.	BCSP	Electrode B current set point	0-100	kA		
11.	AV	Electrode A voltage	<2200	Volts		
12.	BV	Electrode B voltage	<2200	Volts		
13.	AVSP	Electrode A voltage set point	$\leq 2200$	Volts		
14.	BVSP	Electrode B voltage set point	$\leq 2200$	Volts		
15.	AR	Resistance around electrode A	$\geq 0$	$m\Omega$		
16.	BR	Resistance around electrode B	$\geq 0$	$m\Omega$		

Table A1: Overview of process parameters.

To be continued

	Tag	Description	Range	Unit
17.	ARSP	Resistance around electrode A set point	$\geq 0$	mΩ
18.	BRSP	Resistance around electrode B set point	$\geq 0$	$m\Omega$
19.	SER	Specific Energy Ratio	410-440	W/ton
20.	AL	Arc A length		mm
21.	BL	Arc B length		mm
22.	CrucHL	Crucible (the wall) heat loss	0-5	MW
23.	RoofHL	Roof heat loss	0-5	MW
24.	PCHL	Plain cooler heat loss	$\geq 0$	MW
25.	UWCHL	Upper chilled water heat loss	$\geq 0$	MW
26.	LWCHL	Lower chilled water heat loss	$\geq 0$	MW
27.	HFansHL	Hearth (Fans) heat loss	$\geq 0$	MW
28.	HTCsHL	Hearth (Technological Control System) heat loss	$\geq 0$	MW
29.	SL	Slag level		mm
30.	ML	Metal level		mm
31.	FOGET	Off-gas temperature	180-630	°C
32.	TPA	Slag tap A valve opening	0-100	%
33.	TPB	Slag tap B valve opening	0-100	%
34.	CO2	CO <sub>2</sub> volume	0-25	%
35.	ST	Slag temperature after being tapped		°C
Fur	nace feed para	umeters		
36.	FF	Furnace feed rate	0-200	tons/hr
37.	FFDiv5APos	Furnace Feed Inlet Diverter 5A Position 1	[0,1]	
38.	FFDiv5BPos	Furnace Feed Inlet Diverter 5B Position 1	[0,1]	
39.	FFDiv5CPos	Furnace Feed Inlet Diverter 5C Position 1	[0,1]	
40.	FFDiv5DPos	Furnace Feed Inlet Diverter 5D Position 1	[0,1]	
41.	FFDiv5EPos	Furnace Feed Inlet Diverter 5E Position 1	[0,1]	
42.	FFDiv5FPos	Furnace Feed Inlet Diverter 5F Position 1	[0,1]	
43.	W1OC	Weir 1 valve opening	[0,1]	
44.	W2OC	Weir 2 valve opening	[0,1]	
45.	W3OC	Weir 3 valve opening	[0,1]	
46.	W4OC	Weir 4 valve opening	[0,1]	
47.	W5OC	Weir 5 valve opening	[0,1]	
48.	W6OC	Weir 6 valve opening	[0,1]	
49.	W7OC	Weir 7 valve opening	[0,1]	

Table A1 (continued)

To be continued

	Tag	Description	Range	Unit
50.	W8OC	Weir 8 valve opening	[0,1]	
51.	W1F	Weir 1 flow rate	0-200	tons/hr
52.	W2F	Weir 2 flow rate	0-200	tons/hr
53.	W3F	Weir 3 flow rate	0-200	tons/hr
54.	W6F	Weir 6 flow rate	0-200	tons/hr
55.	W7F	Weir 7 flow rate	0-200	tons/hr
56.	W8F	Weir 8 flow rate	0-200	tons/hr
57.	W1	Weir 1 flow rate	$\geq 0$	mA
58.	W2	Weir 2 flow rate	$\geq 0$	mA
59.	W3	Weir 3 flow rate	$\geq 0$	mA
60.	W4	Weir 4 flow rate	$\geq 0$	mA
61.	W5	Weir 5 flow rate	$\geq 0$	mA
62.	W6	Weir 6 flow rate	$\geq 0$	mA
63.	W7	Weir 7 flow rate	$\geq 0$	mA
64.	W8	Weir 8 flow rate	$\geq 0$	mA
65.	TMF	Total microwave flow rate	$\geq 0$	mA
66.	W1T	Feed temperature after leaving weir 1		°C
67.	W2T	Feed temperature after leaving weir 2		°C
68.	W3T	Feed temperature after leaving weir 3		°C
69.	W4T	Feed temperature after leaving weir 4		°C
70.	W5T	Feed temperature after leaving weir 5		°C
71.	W6T	Feed temperature after leaving weir 6		°C
72.	W7T	Feed temperature after leaving weir 7		°C
73.	W8T	Feed temperature after leaving weir 8		°C
74.	IT1	Feed temperature in the distribution bin 1		°C
75.	IT2	Feed temperature in the distribution bin 2		°C
76.	IT3	Feed temperature in the distribution bin 3		°C
77.	IT4	Feed temperature in the distribution bin 4		°C
78.	PAT	Feed temperature entering port A		°C
79.	PB1T	Feed temperature entering port B1		°C
80.	PB2T	Feed temperature entering port B2		°C
81.	PB3T	Feed temperature entering port B3		°C
82.	PB4T	Feed temperature entering port B4		°C
83.	PB5T	Feed temperature entering port B5		°C

Table A1 (continued)

To be continued

	Tag	Description	Range	Unit
84.	PB6T	Feed temperature entering port B6		°C
85.	PC1T	Feed temperature entering port C1		°C
86.	PC2T	Feed temperature entering port C2		°C
87.	PC3T	Feed temperature entering port C3		°C
88.	PC4T	Feed temperature entering port C4		°C
89.	PC5T	Feed temperature entering port C5		°C
90.	PC6T	Feed temperature entering port C6		°C
91.	PC7T	Feed temperature entering port C7		°C
92.	PC8T	Feed temperature entering port C8		°C
93.	PC9T	Feed temperature entering port C9		°C
94.	PC10T	Feed temperature entering port C10		°C
95.	WBCVPF	Weigh bin cone valve position feedback	$\geq 0$	mA
96.	WBCVOMV	Weigh Bin Cone valve opening (Measured Value)	0-100	%
97.	WBCVPCO	Weigh Bin cone valve position controller output	$\geq 0$	mA
98.	CVPCSP	Cone valve position controller set point	0-100	%
99.	FFPAPAF	Furnace feed pipe A, A-port flow	$\geq 0$	tons/hr
Red	uction parame	ters		
100	. FBRLSP	Fluidized bed reducer level set point		m
101	. FBRL	Fluidized bed reducer level		m
102	. FBRCMV	Fluidized bed reducer level		mA
103	FBRLCO	Fluidized bed reducer level controller output	$\geq 0$	mA
104	. FBRCVC	Fluidized bed reducer cone valve control	0-100	%
105	.FBRBedT	Fluidized bed reducer temperature	800-1100	°C
Cale	cining parame	ters		
106	. CalcFR	Calciner feed rate	$\geq 0$	tons/hr
107	. CoalFeed	Coal feed rate	$\geq 0$	tons/hr
Lab	oratory param	eters		
108	. AL2O3	$Al_2O_3$ concentration in the slag		ppm
109	. FeO	FeO concentration in the slag		ppm
110	. MgO	MgO concentration in the slag		ppm
111	. Ni	Ni concentration in the slag		ppm
112	. SiO2	SiO <sub>2</sub> concentration in the slag		ppm

Table A1 (continued)

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